

Università degli Studi di Cagliari





Robust distributed control of multi-agent systems with application to electrical networks

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All we're saying is give peace a chance (J. Lennon 1975)

Summary

- Introduction to Multi-Agent Systems
- Centralised vs Decentralised control
- Consensus in Decentralised control
- Decentralised Leader-following
- Robust Consensus
- Consensus in electrical networks

Multi-Agents System: A complex system composed by several interconnected agents that exchange information and/or materials



Multi-Agents System: A complex system composed by several interconnected agents that exchange information and/or materials

vertex set

edge set

adjacency matrix

G = (V, E, A)

 $V = \{1, 2, \dots, N\}$ $E \subset V \times V$ $A = \begin{bmatrix} a_{i,j} \end{bmatrix} \in \mathbb{R}^{N \times N}_{> 0}$

 $\mathcal{N}_{in} = \{ j \in V : (j, i) \in E \}$

set of in – neighbourhoods of vertex *i* set of out – neighbourhoods $\mathcal{N}_{out} = \{ j \in V : (i, j) \in E \}$ of vertex *i* in – degree matrix out – degree matrix

 $L = \begin{bmatrix} l_{i,j} \end{bmatrix} = D_{out} - A \in \mathbb{R}^{N \times N}$

 $D_{in} = diag(A^T \cdot 1_N)$

 $D_{out} = diag(A \cdot 1_N)$

laplacian matrix



Multi-Agents System: A complex system composed by several interconnected agents that exchange information and/or materials

G = (V, E, A)

The Laplacian matrix is semi-definite positive

$$eig(L) = \{\lambda_1, \lambda_2, \dots, \lambda_n\}$$

$$0 = \lambda_1 \leq \lambda_2 \leq \lambda_3 \leq \ldots \leq \lambda_{\mathsf{N}}$$

 λ_2 gives info on the graph connectivity

 $\lambda_2 > 0 \Rightarrow$ the graph is connected



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The existence of spanning-trees implies connectivity



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A graph is undirected if $(i,j) \in E \Leftrightarrow (i,i) \in E$ $\downarrow \downarrow$ matrices A and L are symmetric if the connected agents have the same "authority" $a_{i,j} = a_{j,i}$



Agents' dynamics: each agent's dynamics depends on the interaction with its in-neighbourhoods

$$\dot{\mathbf{x}}_{i}(t) = \mathbf{F}_{i}(\mathbf{x}_{i}(t), t) + \mathbf{G}_{i}(\mathbf{x}_{i}(t), t) \cdot \mathbf{u}_{i} + \sum_{j \in \mathcal{N}_{i}} a_{j,i} \mathbf{F}_{i,j}(\mathbf{x}_{i}(t))$$

 \mathbf{x}_i : the n_i -dimensional state of the i^{th} agent

- \boldsymbol{u}_i : the m_i -dimensional control of the i^{th} agent
- F_i: the n_i-dimensional vector field of the ith agent's autonomous dynamics
- G_i : the $n_i \times m_i$ -dimensional gain matrix of the *i*th agent
- Γ_i : the $n_{i^{X}}m_{j}$ -dimensional vector function of the j^{th} agent's influence on the i^{th} agent
- $a_{j,i}$: the weight of the connection between the j^{th} and i^{th} agents

Agents' dynamics: each agent's dynamics depends on the interaction with its in-neighbourhoods

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The state of the in-neighbourhoods generally affects the dynamics of the agent in an unmatched way

$$\Gamma_{i,j}(x_j(t), t) \neq G_i(x_i(t), t) \cdot \lambda_j(x_j(t), t)$$

The control and estimation problems become complex

Collective Multi-Agents System: the overall behaviour can have a high-dimensional dynamics

$$\dot{x} = F(x(t), t) + diag\{G_i(x(t), t)\} \cdot u(t) + A \otimes \Gamma(x(t))\}$$

$$\begin{aligned} \mathbf{x}(t) = \begin{bmatrix} x_{1}(t) \\ \vdots \\ x_{N}(t) \end{bmatrix} \mathbf{u}(t) = \begin{bmatrix} u_{1}(t) \\ \vdots \\ u_{N}(t) \end{bmatrix} F(\mathbf{x}(t), t) = \begin{bmatrix} F_{1}(x_{1}(t), t) \\ \vdots \\ F_{N}(x_{N}(t), t) \end{bmatrix} \\ \Gamma(\mathbf{x}(t)) = \begin{bmatrix} 0 & \Gamma_{1,2}(x_{2}(t)) & \dots & \Gamma_{1,N}(x_{N}(t)) \\ \Gamma_{2,1}(x_{1}(t)) & 0 & & \Gamma_{2,N}(x_{N}(t)) \\ \vdots & \ddots & \vdots \\ \Gamma_{N,1}(x_{1}(t)) & \dots & \Gamma_{N,N-1}(x_{N-1}(t)) & 0 \end{bmatrix} \end{aligned}$$

The control and estimation problems become complex

Multi-Agents System: many examples in practice

- Power distribution (i.e. Smart Grids)
- Coordination of mobile robots (i.e. UAVs)
- Sensing in wide areas (i.e. WSN)
- Social Networks (opinion dynamics)
- Traffic control
- Communication networks (routing)









Multi-Agents System: many examples in practice



Different graphs can represent the physical interaction and the communication among the agents

Multi-Agents System: the overall behaviour can have a high-dimensional dynamics

 $\dot{x} = F(x(t), t) + diag\{G_i(x(t), t)\} \cdot u(t) + A \otimes \Gamma(x(t))\}$

- The overall dynamics **IS NOT** a combination of the single agents' dynamics
- Emerging behaviours appear in uncontrolled MAS
- A centralised state-feedback control could solve the problem of imposing a behaviour to the MAS

Centralised control: All measurements are collected by a central agent that defines the control law for all the connected agents considering the overall system condition



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Decentralised control: Each agent has its own control based on its own measurement and some data from its neighbors; same information are shared



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Optimization be can obtained by combining the optimization of a set of locally defined indexes, taking into account neighbors

$$J(\hat{\boldsymbol{u}}) = \sum_{i=1}^{N} \min_{\boldsymbol{u}_{i} \in U_{i}} \int_{t=t_{0}}^{t} L_{i}(\boldsymbol{y}_{i}; \boldsymbol{u}_{i}; \boldsymbol{x}_{j}) dt$$

Consensus: all agents converge to a common behaviour



Consensus: all agents converge to a common behaviour

$$\lim_{t \to \infty} \|x_i - x_j\| = 0; \qquad \forall i \neq j; \ i, j = 1, \dots, N$$

In case of formation control the systems' state don't converge to a common value but a prescribed offset is required

$$\lim_{t \to \infty} \|x_i - x_j\| = d_{i,j}; \qquad \forall i \neq j; \ i, j = 1, \dots, N$$



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Wei Ren, Randal W. Beard, Ella M. Atkins. A Survey of Consensus Problems in Multi-agent Coordination, Proceedings of the American Control Conference, Volume 3, Pages 1859 – 1864, 2005.

Reza Olfati-Saber, J. Alex Fax, Richard M. Murray. Consensus and Cooperation in Networked Multi-Agent Systems, Proceedings of the IEEE, Volume: 95, Issue: 1, January 2007.

Some references

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- M. Mesbahi, M. Egerstedt. *Graph Theoretic Methods for Multiagent Networks*, Princeton University Press, Princeton, NJ, 2010
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- Fagnani F., Zampieri S., Randomized consensus algorithms over large scale networks, IEEE Journal on Selected Areas in Communications, 26(4), pp. 634-649, 2008
- Dörfler F., Bullo F., Synchronization in complex networks of phase oscillators: A survey, Automatica, 50(6), pp. 1539-1564, 2014

The most simple consensus decentralised control problem refers to a single or double integrator agent

$$\dot{x}_i = u_i$$
 or $\ddot{x}_i = u_i$ $i=1,2,...,N$

- Single integrator: *velocity driven agent*
- Double integrator: *acceleration driven agent*

In the case of **single integrators**, the control of each agent can be defined to "modify" the strength of the connection between neighbour agents

$$u_{i} = -\sum_{j \in \mathcal{N}_{out_{i}}} a_{j,i} (x_{i} - x_{j})$$
 $i = 1, 2, ..., N$

The MAS dynamics results into

$$\dot{x} = -L \cdot x$$

A. Jadbabaie, J. Lin, and A. S. Morse, "Coordination of groups of mobile autonomous agents using nearest neighbor rules," IEEE Trans. on Automatic Control, vol. 48, pp. 988–1001, June 2003

Considering single integrator agents

The MAS dynamics results into

 $\dot{x} = -L \cdot x$

Because of the semi-positive definiteness of the Laplacian matrix L, the state of a **connected MAS** converge to a, generally not zero, globally exponentially stable state

 $x \rightarrow \alpha \cdot \mathbf{1};$

The α value depends on the coefficients of the adjacency matrix A

Considering single integrator agents

The MAS dynamics results into

$$\dot{x} = -L \cdot x$$





Considering single integrator agents

The MAS dynamics results into

$$\dot{x} = -L \cdot x$$



If the graph is strongly connected and doubly stochastics α is the **mean value** of the agents' initial state



Considering single integrator agents

The MAS dynamics results into

$$\dot{x} = -L \cdot x$$



The larger the coupling coefficients the shorter the convergence, i.e λ_2 increases



Considering single integrator agents

The MAS dynamics results into

 $\dot{x} = -L \cdot x$

Stability can be proved by a disagreement function

Gradient descent algorithm on a convex definite positive function

J. Cortés, "Finite-time convergent gradient flows with applications to network consensus," Automatica, vol. 42, no. 11, pp. 1993–2000, 2006.

Considering double integrator agents

The MAS dynamics results into

$$\dot{x}_{i,1} = x_{i,2}$$

 $\dot{x}_{i,2} = u_i$
 $i = 1, 2, ..., N$

Also in the case of **double integrators**, the control of each agent can be defined to "modify" the strength of the connection between neighbour agents , which exchange both position and velocity variables

$$u_{i} = -\sum_{i \in \mathcal{N}_{out_{i}}} a_{j,i} \left(x_{i,1} - x_{j,1} \right) - \lambda \sum_{i \in \mathcal{N}_{out_{i}}} a_{j,i} \left(x_{i,2} - x_{j,2} \right)$$

W. Ren and E. M. Atkins, "Distributed multi-vehicle coordinated control via local information exchange," Int. J. Robust Nonlinear Contr., vol. 17, no. 10– 11, pp. 1002–1033, Jul. 2007

Considering double integrator agents

The MAS dynamics results into

$$\begin{bmatrix} \dot{\mathbf{x}}_1 \\ \dot{\mathbf{x}}_2 \end{bmatrix} = \begin{bmatrix} 0 & I \\ -L & -\lambda L \end{bmatrix} \begin{bmatrix} \mathbf{x}_1 \\ \mathbf{x}_2 \end{bmatrix}$$

Since the Laplacian L is a semi-definite positive matrix with a unique zero eigenvalue if the graph is fully connected, the MA dynamics' matrix has a double eigenvalue in zero and all the others have negative real part.

$$x_1 \to \alpha_1 \cdot 1 + \alpha_2 \cdot 1t$$
$$x_2 \to \alpha_2 \cdot 1$$

Coefficients α_1 and α_2 are weighted values of the initial position and velocity of the agents, and depend on the entries of matrix A

Considering double integrator agents

The MAS dynamics results into







Considering double integrator agents

The MAS dynamics results into



Parameter λ affects the transient behaviour



Considering double integrator agents

The MAS dynamics results into









Decentralised Leader-following

Some of the agents act independently from the others


Some of the agents act independently from the others They are the root of spanning trees









The MA dynamics can be represented by a "classic" interaction dynamics plus an external reference



Single integrator case

Leader's velocity propagates as a **disturbances** in agents'dynamics

Even tracking for the agent connected to the leader is lost

The MA dynamics should be represented by a switching interaction dynamics plus an external reference



Single integrator case

$$\dot{x}_{0} = -a_{0}x_{0} + u_{0}$$

$$\dot{x} = sign\left(\begin{bmatrix} a_{1,0} \\ 0 \end{bmatrix} - \overline{L} \end{bmatrix} \cdot \begin{bmatrix} x_{0} \\ x \end{bmatrix} \right)$$

$$\overline{L} = \begin{bmatrix} a_{1,0} & 0 \\ 0 & 0 \end{bmatrix} + L$$



The MA dynamics should be represented by a switching interaction dynamics plus an external reference



Single integrator case

The gain of the switching interactions must be large enough



The MA dynamics can be represented by a "classic" interaction dynamics plus an external reference



 $a_0=1, a_1=1, u_0=4 \delta_1(t-10)$ $a_{1,0}=1 \lambda=2$

The MA dynamics can be represented by a "classic" interaction dynamics plus an external reference



Double integrator case

Leader's velocity and control propagates as a **disturbances** in agents'dynamics

Even tracking for the agent connected to the leader is lost

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$$\begin{cases} \dot{x}_{0_{1}} = x_{0_{2}} \\ \dot{x}_{0_{2}} = -a_{0}x_{0_{1}} - a_{1}x_{0_{2}} + u_{0} \\ \\ \dot{x}_{1} = x_{2} \\ \dot{x}_{2} = \alpha \cdot sign \left(\left[\begin{bmatrix} a_{1,0} \\ 0 \end{bmatrix} - \overline{L} \right] \cdot \begin{bmatrix} x_{0} \\ x_{1} \end{bmatrix} \right) + \lambda \cdot sign \left(\left[\begin{bmatrix} a_{1,0} \\ 0 \end{bmatrix} - \overline{L} \right] \cdot \begin{bmatrix} \dot{x}_{0} \\ x_{2} \end{bmatrix} \right) \\ \overline{L} = \begin{bmatrix} a_{1,0} & 0 \\ 0 & 0 \end{bmatrix} + L$$

- The leader's trajectory becomes an equilibrium movement of the MAS
- Consensus with tracking is reached in a finite time
- The drift due to the integrative effect between velocity and position is eliminated
- Controller tuning depends on the characteristics of the movement of the leader

Single integrators case with formation control



Agents' dynamics is affected by uncertainty

- Uncertain drift term
- Disturbances
- Measurement noise
- Unmodelled dynamics
- Switching topology of the net
- Communication delays
- Packets' jittering
- Packets' loss

In order to deal with such a number of *"accidents"* assumptions should be made to find solutions

Robustness is an issue in MAS control and VSC could help!

- Uncertain drift term
- Disturbances
- Measurement noise
- Unmodelled dynamics
- Switching topology of the net
- Communication delays
- Packets' jittering
- Packets' loss
- Adverse agents

Just some of the "accidents" will be considered now on

Agents' dynamics is affected by uncertainty

Agents are 1th order systems

Agents are 2ndorder systems

 $\dot{x}_i = f_i(x_i, t) + u_i$

$$\dot{x}_{i_1} = x_{i_2}$$

 $\dot{x}_{i_2} = f_i(x_i, t) + u_i$

The uncertain drift should fulfil some requirements, e.g., boundedness, continuity, lipshitzness, etc

Agents are 1th order systems

$$u_i = -\alpha \cdot sign\left(\sum_{j \in N_{out_i}} \left(x_i - x_j\right)\right)$$

$$\dot{x}_{i} = f_{i}(x_{i}, t) + u_{i}$$
$$\alpha > \Phi \ge |F(x, t)|_{\infty}$$

 $f_{1} = \sin(t)$ $f_{2} = 0.5 \sin(3t)$ $f_{3} = \sin((0.2+0.6t)t)$ $f_{4} = 0$ $f_{5} = \delta_{-1}(t-10)$

A control depending on the bounds of the uncertainty could help and compensate for the uncertainty

α= 3





Agents are 1th order systems $\dot{x}_i = f_i(x_i, t) + u_i$

$$u_i(t) = -\alpha \cdot \sum_{j \in \mathcal{N}_i} (x_i(t) - x_j(t)) - \beta \cdot \operatorname{SIGN}(x_i(t) + z_i(t))$$
$$\dot{z}_i(t) = \alpha \cdot \sum_{j \in \mathcal{N}_i} (x_i(t) - x_j(t)), \qquad z_i(0) = -x_i(0)$$

Defining the "sliding variable" $\boldsymbol{\sigma}(t) = \boldsymbol{x}(t) + \boldsymbol{z}(t)$ $\dot{\boldsymbol{x}}(t) = \boldsymbol{w}(t) - \boldsymbol{\alpha} \cdot \boldsymbol{\mathcal{L}} \boldsymbol{x}(t) - \boldsymbol{\beta} \cdot \text{SIGN}(\boldsymbol{\sigma}(t))$ $\dot{\boldsymbol{\sigma}}(t) = \boldsymbol{w}(t) - \boldsymbol{\beta} \cdot \text{SIGN}(\boldsymbol{\sigma}(t)), \quad \boldsymbol{\sigma}(0) = \boldsymbol{0}_n$

A. Pilloni, M. Franceschelli, A. Pisano, E. Usai., Sliding Mode-Based Robustification of Consensus and Distributed Optimization Control Protocols, IEEE TAC, VOL. 66, NO. 3, pp. 1207-1214, 2021





$$\begin{split} \dot{x}_{i} &= \alpha + f_{i}(t) + u_{i} \qquad \left| f_{i}(t) \right| \leq \pi_{i} \leq \max\{\pi_{i}\} = \Pi\\ G(t) &= \{V, E(t), A(t)\} \qquad A(t) = A^{T}(t); \forall t \end{split}$$



$$\begin{split} \dot{x}_{i} &= \alpha + f_{i}(t) + u_{i} \qquad \left| f_{i}(t) \right| \leq \pi_{i} \leq \max\{\pi_{i}\} = \Pi \\ &i \in V \\ G(t) &= \{V, E(t), A(t)\} \qquad A(t) = A^{T}(t); \forall t \end{split}$$

$$u_{i} = -\lambda \sum_{j \in \mathcal{N}_{i}(t)} a_{i,j}(t) \operatorname{sign}\left(x_{i} - x_{j}\right) \qquad \lambda \ge \frac{|E|\Pi T + \mu^{2}}{\varepsilon}; \mu \neq 0$$

|E| is the cardinality of the set containing all possible edge of the time-varying graph

$$\left| x_{i} - x_{j} \right| \leq 2|E|\Pi(T - \varepsilon); \quad \forall t \geq \frac{T}{2\mu^{2}} \sum_{(i,j) \in E} \left| x_{i_{0}} - x_{j_{0}} \right|$$

Franceschelli M., Giua A., Pisano A., Usai E., Finite-Time Consensus for Switching Network Topologies with Disturbances, Nonlinear Analysis: Hybrid Systems, vol. 10, pp. 83-93, 2014.

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$$\begin{split} \dot{x}_{i} &= \alpha + f_{i}(t) - \lambda \sum_{j \in \mathcal{N}_{i}(t)} a_{i,j}(t) \ sign\left(x_{i} - x_{j}\right) \\ G(t) &= \{V, E(t), A(t)\} \qquad A(t) = A^{T}(t); \ \forall t \qquad E(t) \subset E \ \forall t \end{split}$$

- Number of clocks: 20.
- Topology: a random graph.
- Sampling step: 0.1 milliseconds.
- Desired clock speed: $\alpha = 1$
- Initial clocks bias chosen uniformly at random within [0,1].
- Disturbance model: $\nu_i(t) = \frac{5}{2}(n_i(t) + \sin(3|n_i(t)|t))$
- *n_i(t)* ∈ [−1,1] is a uniformly distributed random variable for any *t*.
 λ = 30

$$\dot{x}_{i} = \alpha + f_{i}(t) - \lambda \sum_{j \in \mathcal{N}_{i}(t)} a_{i,j}(t) \operatorname{sign}(x_{i} - x_{j})$$
$$G(t) = \{V, E(t), A(t)\} \qquad A(t) = A^{T}(t); \forall t \qquad E(t) \subset E \forall t$$



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Convergence to the median value is more robust in the presence of adverse agents

$$\dot{x}_i = u_i$$

Agent	value	Attack 1	Attack 2	Attack 3	Attack 4	Attack 5	Attack 6
1	4	8	4	4	4	4	4
2	0	0	0	0	0	0	0
3	3	3	3	3	3	3	3
4	2	2	2	2	2	2	2
5	-1	-1	-4	-1	-1	-1	-1
6	1	1	1	4	1	1	1
7	1	1	1	1	1	1	1
8					5	2	-3
mean	1,43	2,00	1,00	1,86	1,88	1,50	0,88
median	1,00	1,00	1,00	2,00	1,50	1,50	1,00

Convergence to the median value is more robust in the presence of adverse agents

$$\begin{aligned} x_{i} &= -\alpha_{i} sign\left(x_{i} - x_{i_{0}}\right) - \sum_{j \in \mathcal{N}_{i}} \lambda_{i,j} sign\left(x_{i} - x_{j}\right) & \lambda_{i,j} = \lambda_{j,i} \quad \forall \ (i,j) \in E \\ \lambda_{i,j} &> 0 \quad 0 < \max_{i \in V} \{\alpha_{i}\} < \frac{2k \min_{\substack{(i,j) \in E}} \{\lambda_{i,j}\}}{N} \\ \max\{x_{\cdot}\} - \min\{x_{\cdot}\} \end{aligned}$$

$$\begin{aligned} |x_i - x_{i_0}| &\longrightarrow \\ t \to T \end{aligned} \qquad T \leq \frac{T \leq \frac{1}{i \in V} \left(\frac{1}{i_0} \right) - \frac{1}{i \in V} \left(\frac{1}{i_0} \right)}{2 \left(\frac{2k \min \{\lambda_{i,j}\}}{N} - \max \{\alpha_i\} \right)} \end{aligned}$$

k is the maximum number of vertex that can be eliminated maintain a connected graph

M. Franceschelli, A. Giua, A. Pisano, "Finite-Time Consensus on the Median Value with Robustness Properties," IEEE Trans. on Automatic Control, Vol. 62, No. 4, pp. 1652-1667, 2017

Convergence to the median value is more robust in the presence of adverse agents

Once the consensus is reached the states are driven to the median value provided that

$$\frac{\max\{\alpha_i\} - \min\{\alpha_i\}}{\substack{i \in V \\ min\{\alpha_i\} \\ i \in V}} < \frac{1}{N}$$

$$x_{i} \xrightarrow{t \to T_{2}} m(x_{0}) = \begin{cases} z & \text{if } N \text{ is odd} \\ N/2+1 & T_{2} \end{cases} \qquad T_{2} \leq T + 2N \frac{\left| x_{i}(T) - m(x_{0}) \right|}{\max_{i \in V}} \\ \left[z & z_{N/2} & N/2+1 \right] & \text{if } N \text{ is even} \end{cases}$$

M. Franceschelli, A. Giua, A. Pisano, "Finite-Time Consensus on the Median Value with Robustness Properties," IEEE Trans. on Automatic Control, Vol. 62, No. 4, pp. 1652-1667, 2017

Convergence to the median value is more robust in the presence of adverse agents



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Convergence to the median value is more robust in the presence of adverse agents





A physical network connecting:

- Generation systems
- Loads
- Storages

Increasing the renewable energies production introduces strong variability in generation systems

Loads are uncertain

Generation and loads must be balanced in a very short time



Main control issues

- Stability and Power sharing
- Frequency and voltage restoration
- Dispatching of power flows

Dispatching of power flows

Usually, but not only, based on centralised heuristic optimization methods

Gan, D., Thomas, R.J., Zimmerman, R.D., Stability-constrained optimal power flow, IEEE Transactions on Power Systems, 15(2), pp. 535-540, 2000

Borges, C.L.T., Falcão, D.M., Optimal distributed generation allocation for reliability, losses, and voltage improvement, International Journal of Electrical Power and Energy Systems, 28(6), pp. 413-420, 2006

Georgilakis, P.S., Hatziargyriou, N.D., Optimal distributed generation placement in power distribution networks: Models, methods, and future research, IEEE Transactions on Power Systems, 28(3), pp. 3420-3428, 2013

Parisio, A., Rikos, E., Glielmo, L., A model predictive control approach to microgrid operation optimization, IEEE Transactions on Control Systems Technology, 22(5), pp. 1813-1827, 2014

Biswas, P.P., Suganthan, P.N., Amaratunga, G.A.J., Optimal power flow solutions incorporating stochastic wind and solar power, Energy Conversion and Management, 148, pp. 1194-1207, 2017

Rinaldi, G., Menon, P.P., Edwards, C., Ferrara, A., Sliding Mode Observer-Based Finite Time Control Scheme for Frequency Regulation and Economic Dispatch in Power Grids, IEEE Transactions on Control Systems Technology, 30(3), pp. 1296-1303, 2022

Frequency and voltage restoration

Nowadays most approaches are based on MAS theory

Shafiee Q., Guerrero J.M., Vasquez J.C., Distributed secondary control for islanded microgrids-a novel approach, IEEE Transactions on Power Electronics, 29(2), pp. 1018-1031, 2014

Guo F., Wen C., Mao J., Song Y.-D., Distributed Secondary Voltage and Frequency Restoration Control of Droop-Controlled Inverter-Based Microgrids, IEEE Transactions on Industrial Electronics, 62(7), pp. 4355-4364, 2015

J. Schiffer, T. Seel, J. Raisch, T. Sezi, Voltage stability and reactive power sharing in inverter-based microgrids with consensus-based distributed voltage control, IEEE Transactions on Control Systems Technology, 24(1), pp. 96 - 109, 2016

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Stability and Power sharing

Most approaches are based on droop control

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Stability and Power sharing

Most approaches are based on droop control



The presence of **converter** based connections between generators and the network allows for minimizing the load effects on the system dynamics

Modelling the network



The presence of interacting physical and communication networks makes an electrical network a multi-agent cyberphysical system

Modelling the network

ω_{com}	Speed of the common rotating ref. frame
ω_i	Local rotating ref. frame's speed of the <i>i</i> -th DG
δ_i	Angle between the local and the common ro-
	tating ref. frame, i.e., $\dot{\delta}_i = \omega_i - \omega_{com}$
$\omega_{ni}, \upsilon_{ni}$	Frequency and voltage droop-power setpoints
v_{ki}, i_{ki}	3-ph voltages, currents at node k of the <i>i</i> -th DG
v_{kdi}, v_{kqi}	d-q voltages of the i -th DG at node k
ikdi, ikqi	d-q currents of the <i>i</i> -th DG at node k
k = l, o, b	input, output and branch local node of a DG
$\overline{\omega}, \overline{\upsilon}$	Rated values of MG's frequency and voltage
$\omega_{ref}, \upsilon_{ref}$	Desired values of frequency and voltage
P_i, Q_i	Active and reactive powers dc-components at
	the output node of the <i>i</i> -th DG
v_{odi}^*, v_{oqi}^*	d-q voltage setpoints of the <i>i</i> -th DG
ψ_{di}, ψ_{qi}	d-q voltage error's integral of the <i>i</i> -th DG
i_{ldi}^*, i_{lai}^*	d-q current setpoints of the <i>i</i> -th DG
ϕ_{di}, ϕ_{qi}	d-q current error's integral of the <i>i</i> -th DG

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Modelling the network

Frequency dynamics

Power droop control

Active and reactive power (measured)

Voltage primary PI control

$$\frac{d o_i}{dt} = \omega_i - \omega_{\rm com}$$
$$\omega_i = \omega_{ni} - m_i \cdot P_i$$

$$v_{odi}^* = v_{ni} - n_i \cdot Q_i$$
$$v_{oqi}^* = 0$$

$$\frac{dP_i}{dt} = -\omega_{ci}P_i + \omega_{ci}\left(\upsilon_{odi} \cdot i_{odi} + \upsilon_{oqi} \cdot i_{oqi}\right)$$
$$\frac{dQ_i}{dt} = -\omega_{ci}Q_i + \omega_{ci}\left(\upsilon_{oqi} \cdot i_{odi} - \upsilon_{odi} \cdot i_{oqi}\right)$$

$$\begin{aligned} \frac{d\psi_{di}}{dt} &= k_{ivi}(\upsilon_{odi}^* - \upsilon_{odi}) \\ \frac{d\psi_{qi}}{dt} &= k_{ivi}(\upsilon_{oqi}^* - \upsilon_{oqi}) \\ i_{ldi}^* &= \psi_{di} + k_{pvi}(\upsilon_{odi}^* - \upsilon_{odi}) + k_{fvi}i_{odi} - \overline{\omega}C_{fi}\upsilon_{oqi} \\ i_{lqi}^* &= \psi_{qi} + k_{pvi}(\upsilon_{oqi}^* - \upsilon_{oqi}) + k_{fvi}i_{oqi} + \overline{\omega}C_{fi}\upsilon_{odi} \end{aligned}$$

Modelling the network

Current primary PI control

$$\begin{aligned} \frac{d\phi_{di}}{dt} &= k_{ici}(i_{ldi}^* - i_{ldi}) \\ \frac{d\phi_{qi}}{dt} &= k_{ici}(i_{lqi}^* - i_{lqi}) \\ \upsilon_{ldi}^* &= \phi_{di} + k_{pci}(i_{ldi}^* - i_{ldi}) - \overline{\omega}L_{fi}i_{lqi} \\ \upsilon_{lqi}^* &= \phi_{qi} + k_{pci}(i_{lqi}^* - i_{lqi}) + \overline{\omega}L_{fi}i_{ldi} \end{aligned}$$

LC filter and output connector

$$\begin{aligned} \frac{di_{ldi}}{dt} &= -\frac{R_{fi}}{L_{fi}}i_{ldi} + \frac{1}{L_{fi}}\left(\upsilon_{ldi} - \upsilon_{odi}\right) + \omega_{i}i_{lqi} \\ \frac{di_{lqi}}{dt} &= -\frac{R_{fi}}{L_{fi}}i_{lqi} + \frac{1}{L_{fi}}\left(\upsilon_{lqi} - \upsilon_{oqi}\right) - \omega_{i}i_{ldi} \\ \frac{d\upsilon_{odi}}{dt} &= \frac{1}{C_{fi}}\left(i_{ldi} - i_{odi}\right) + \omega_{i}\upsilon_{lqi} \\ \frac{d\upsilon_{oqi}}{dt} &= \frac{1}{C_{fi}}\left(i_{lqi} - i_{oqi}\right) - \omega_{i}\upsilon_{ldi} \\ \frac{di_{odi}}{dt} &= -\frac{R_{ci}}{L_{ci}}i_{odi} + \frac{1}{L_{ci}}\left(\upsilon_{odi} - \upsilon_{bdi}\right) + \omega_{i}i_{oqi} \\ \frac{di_{oqi}}{dt} &= -\frac{R_{ci}}{L_{ci}}i_{oqi} + \frac{1}{L_{ci}}\left(\upsilon_{oqi} - \upsilon_{bqi}\right) - \omega_{i}i_{odi} \end{aligned}$$

Modelling the network

$$\begin{aligned} \dot{x}_{i} &= f_{i}(x_{i}) + g_{i}(x_{i}) \cdot u_{i} + w_{i}(x_{i})d_{i} \\ x_{i} &= \left[\delta_{i}, P_{i}, Q_{i}, \phi_{di}, \phi_{qi}, \psi_{di}, \psi_{qi}, i_{ldi}, i_{lqi}, \upsilon_{odi}, \upsilon_{oqi}, i_{odi}, i_{oqi}\right] \\ w_{i} &= \left(\left(\omega_{i} - \overline{\omega}\right)\upsilon_{oqi} + \psi_{di} - k_{pvi}\upsilon_{odi} + (k_{fvi} - 1)i_{odi}\right) \qquad |\dot{w}_{i}| \leq \overline{\Omega}_{i}, \quad \overline{\Omega}_{M} = \max_{i}\overline{\Omega}_{i} \end{aligned}$$



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Control goals

1 - Compensate for frequency and voltage variation

$$\omega_{i} = \omega_{ref}$$

$$\forall i \in V$$

$$v_{od_{i}} = v_{ref}$$

2 – Guarantee the desired power sharing between generators

$$\frac{P_i}{P_k} = \frac{m_k}{m_i} \qquad \forall (i,k) \in E$$

Since $\omega_i = \omega_{ni} - m_i P_i$ frequency restoration \Rightarrow Power sharing by droop control

The control problems can be formulated as two consensus problems

Frequency restoration

$$\begin{split} \omega_{ni} &= \tilde{\omega}_i + \bar{\omega} \\ \dot{\omega}_i &= -\alpha \cdot \operatorname{sign}\left(\sum_{j \in \mathcal{N}_i} \left(\tilde{\omega}_i - \tilde{\omega}_j\right) + \sum_{j \in \mathcal{N}_i} \left(\omega_i - \omega_j\right) + g_i \left(\omega_i - \omega_{ref}\right)\right) \end{split}$$

 $\overline{\omega}$ is the rated nominal MG's frequency

The MAS dynamics results into

$$\dot{\delta} = \omega - \omega_{com} = \tilde{\omega} + \mathbf{1}_n \otimes (\overline{\omega} - \omega_{com}) - \mathbf{m} \cdot \mathbf{P}$$

 $\dot{\tilde{\omega}} = -\alpha \cdot \operatorname{Sign} \left(\mathcal{L} \left(\omega + \tilde{\omega} \right) + \mathbf{G} \left(\omega - \mathbf{1}_n \otimes \omega_{ref} \right) \right)$

A. Pilloni, A. Pisano, E. Usai, Robust Finite Time Frequency and Voltage Restoration of Inverter-based Microgrids via Sliding Mode Cooperative Control, IEEE Trans. on Industrial Electronics, vol. 65, n. 1, pp. 907-917, 2018

The control problems can be formulated as two consensus problems

Frequency restoration

Once the sliding mode is established the MAS dynamics moves along the sliding manifold

$$\sigma_{\omega} = [\sigma_{\omega,i}] = \mathcal{L}\left(\omega + \tilde{\omega}\right) + G\left(\omega - \mathbf{1}_n \otimes \omega_{ref}\right)$$

and the resulting dynamics is

$$\dot{\delta} = \omega - \omega_{com} = \tilde{\omega} + \mathbf{1}_n \otimes (\overline{\omega} - \omega_{com}) - m \cdot P$$

 $\dot{\tilde{\omega}} = -\alpha \cdot \operatorname{Sign} \left(\mathcal{L} \left(\omega + \tilde{\omega} \right) + G \left(\omega - \mathbf{1}_n \otimes \omega_{ref} \right) \right)$

A. Pilloni, A. Pisano, E. Usai, Robust Finite Time Frequency and Voltage Restoration of Inverter-based Microgrids via Sliding Mode Cooperative Control, IEEE Trans. on Industrial Electronics, vol. 65, n. 1, pp. 907-917, 2018

The control problems can be formulated as two consensus problems

Voltage restoration

The agent's dynamics is

$$\frac{d\upsilon_{\text{odi}}}{dt} = w_i(\omega_i, \psi_{di}, \upsilon_{\text{odi}}, \upsilon_{\text{oqi}}, i_{\text{odi}}) + \bar{w}_i \cdot \upsilon_{ni}$$

 v_{ni} is the control variable for the *i*-th agent, and should be continuous

$$\dot{\upsilon}_{ni} = -\frac{C_{fi}}{k_{\text{pvi}}} \left[\varsigma_1 \cdot \text{sign} \left(\sum_{j \in \mathcal{N}_i} \left(\upsilon_{\text{odi}} - \upsilon_{\text{odj}} \right) + g_i \left(\upsilon_{\text{odi}} - \upsilon_{\text{ref}} \right) \right) + \varsigma_2 \cdot \text{sign} \left(\sum_{j \in \mathcal{N}_i} \left(\dot{\upsilon}_{\text{odi}} - \dot{\upsilon}_{\text{odj}} \right) + g_i \left(\dot{\upsilon}_{\text{odi}} - \dot{\upsilon}_{\text{ref}} \right) \right) \right]$$

A. Pilloni, A. Pisano, E. Usai, Robust Finite Time Frequency and Voltage Restoration of Inverter-based Microgrids via Sliding Mode Cooperative Control, IEEE Trans. on Industrial Electronics, vol. 65, n. 1, pp. 907-917, 2018



- MG with 4 generators and four local loads
- Realistic Noisy Measurement with SNR=90dB
- Load changes and faults



TABLE I										
SPECIFICATION OF THE MICROGRID	TEST SYSTEM									

DG's Parameters	DG 1		DG 2	DG 3		DG 4		
Droop Control	m_p n_Q	$\begin{array}{c} 10\times10^{-5}\\ 1\times10^{-2} \end{array}$		$\begin{array}{c} 6\times10^{-5}\\ 1\times10^{-2} \end{array}$	$\begin{array}{c} 4\times10^{-5}\\ 1\times10^{-2} \end{array}$		$\begin{array}{c} 3\times10^{-5} \\ 1\times10^{-2} \end{array}$	
Voltage Control	$k_{pv}\ k_{iv}\ k_{fv}$	v 0.4 iv 500 fv 0.5		0.4 500 0.5	0.4 500 0.5		0.4 500 0.5	
Current Control	$k_{pc} \\ k_{ic}$	0.4 700		0.4 700	0.4 700		0.4 700	
LC Filter [Ω],[mH],[μ F]	$R_f \\ L_f \\ C_f$	f = 0.1 f = 1.35 f = 50		0.1 1.35 50	0.1 1.35 50		0.1 1.35 50	
Connector [\O],[mH]	R_c L_c	0.03 0.35		0.03 0.35	0.03 0.35		0.03 0.35	
Lines [Ω],[μ H]	Line 1		1	Line 2		Line 3		
	R_{l1} L_{l1}	0.23 318	R_{l2} L_{l2}	0.23 324	R_{l3} L_{l3}		0.23 324	
Loads [kW],[kVar]	Load 1		Load 2		Load 3		Load 4	
	$P_{L1} Q_{L1}$	3 1.5	$P_{L2} Q_{L2}$	3 1.5	$P_{L3} Q_{L3}$	2 1.3	$P_{L4} Q_{L4}$	3 1.5



- 1) At the startup (t = 0 s), only the PC is active with PC set-points $\omega_{ni} = 2\pi \cdot 50$ Hz and $\upsilon_{ni} = 220$ V_{RMS} ≈ 380 V_{ph-ph}.
- 2) At t = 5 s the frequency restoration SC (30)–(31) is activated with $\omega_{ref} = 2\pi \cdot 50$ Hz.
- 3) At t = 10 s the voltage restoration SC (39) is activated with $v_{ref} = 220 V_{RMS} \approx 380 V_{ph-ph}$.
- 4) By using a three-phase breaker, Load 3, i.e., (P_{L3}, Q_{L3}) , is connected at t = 15 s, and removed at t = 25 s.
- 5) At t = 30 s the SC frequency setpoint is changed to $\omega_{\text{ref}} = 2\pi \cdot 50.2$ rad/s.
- 6) At t = 35 s the SC voltage setpoint is changed to $v_{ref} = 224 V_{RMS} \approx 388 V_{ph-ph}$.
- 7) At t = 40 s a three-phase to ground fault occurs on the Line 3.
- 8) At t = 40.01 s overcurrent protection devices isolate the Line 3, and thus DG 4 and Load 4, from the MG.
- 9) At t = 42 s the SC is reconfigured to take into account the changes occurred at the physical layer, i.e., $a_{34} = a_{43} = 0$.
- 10) At t = 43 s the SC frequency setpoint is changed to $\omega_{\text{ref}} = 2\pi \cdot 50.2$ rad/s.
- 11) At t = 44 s the SC voltage setpoint gets back to $v_{ref} = 220 V_{RMS} \approx 380 V_{ph-ph}$.





Output voltages' frequencies are well regulated at desired values





Power sharing is obtained as a side-by effect of the frequency restoration

The control in the presence of communication delays among the generators has been recently considered and a solution is presented in

Gholami M.; Pilloni A.; Pisano A.; Usai E., Robust Distributed Secondary Voltage Restoration Control of AC Microgrids under Multiple Communication Delays. *Energies* **2021**, *14*, 1165. https://doi.org/10.3390/en14041165

Preliminary (but not well proved) results on the transition from islanded to grid-connected microgrid by consensus of a MAS with a leader

Summing up

Variable structure control with sliding mode seams to be able to contribute to the development of robust decentralised control of multi agent systems

Peculiar Lyapunov function could be taken into account to prove stability properties of the controlled MAS

Good Work to all!

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Thank you for you attention

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All we're saying is give peace a chance (J. Lennon 1975)